

# **GPS/GLONASS Antennas and Ground Planes: Size and Weight Reduction Perspectives.**

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Results, perspectives and probable  
limitations of GPS/GLONASS/GALILEO  
broadband multipath-protected antennas

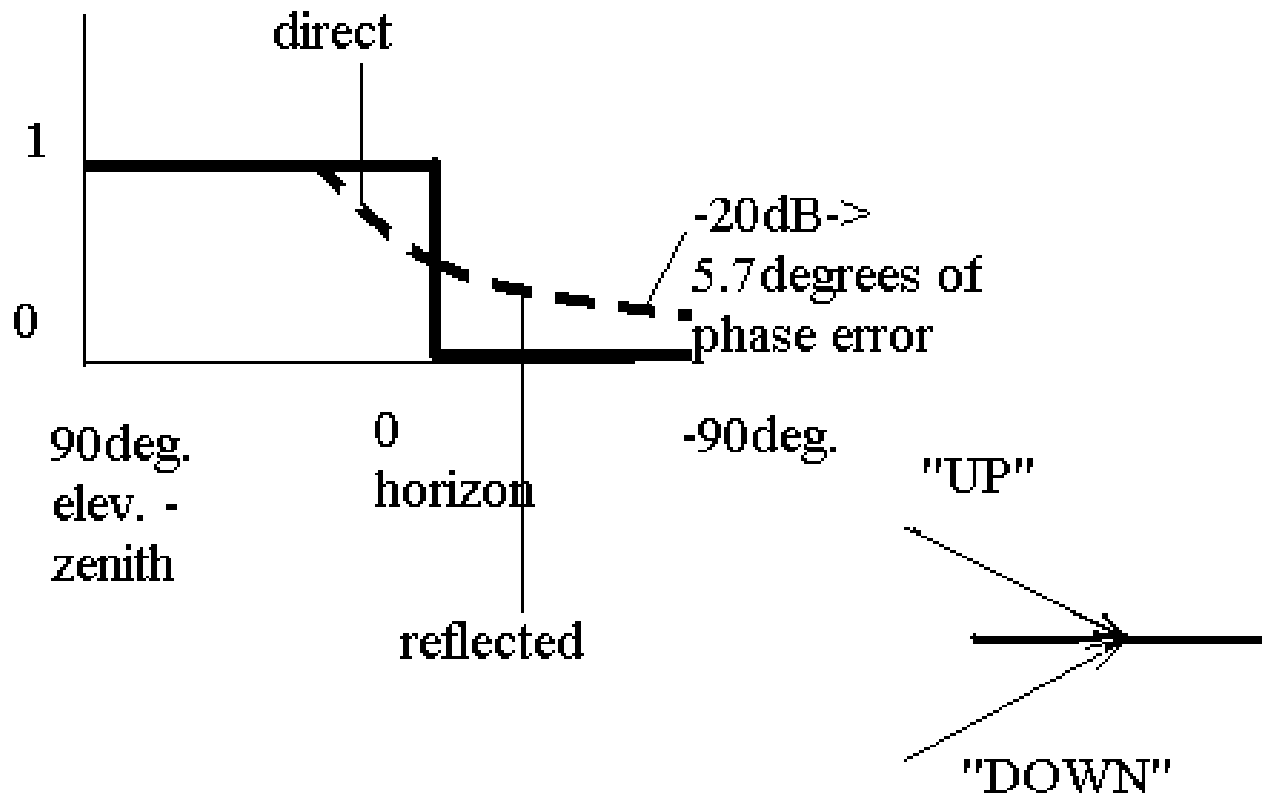
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University of Berne, Switzerland

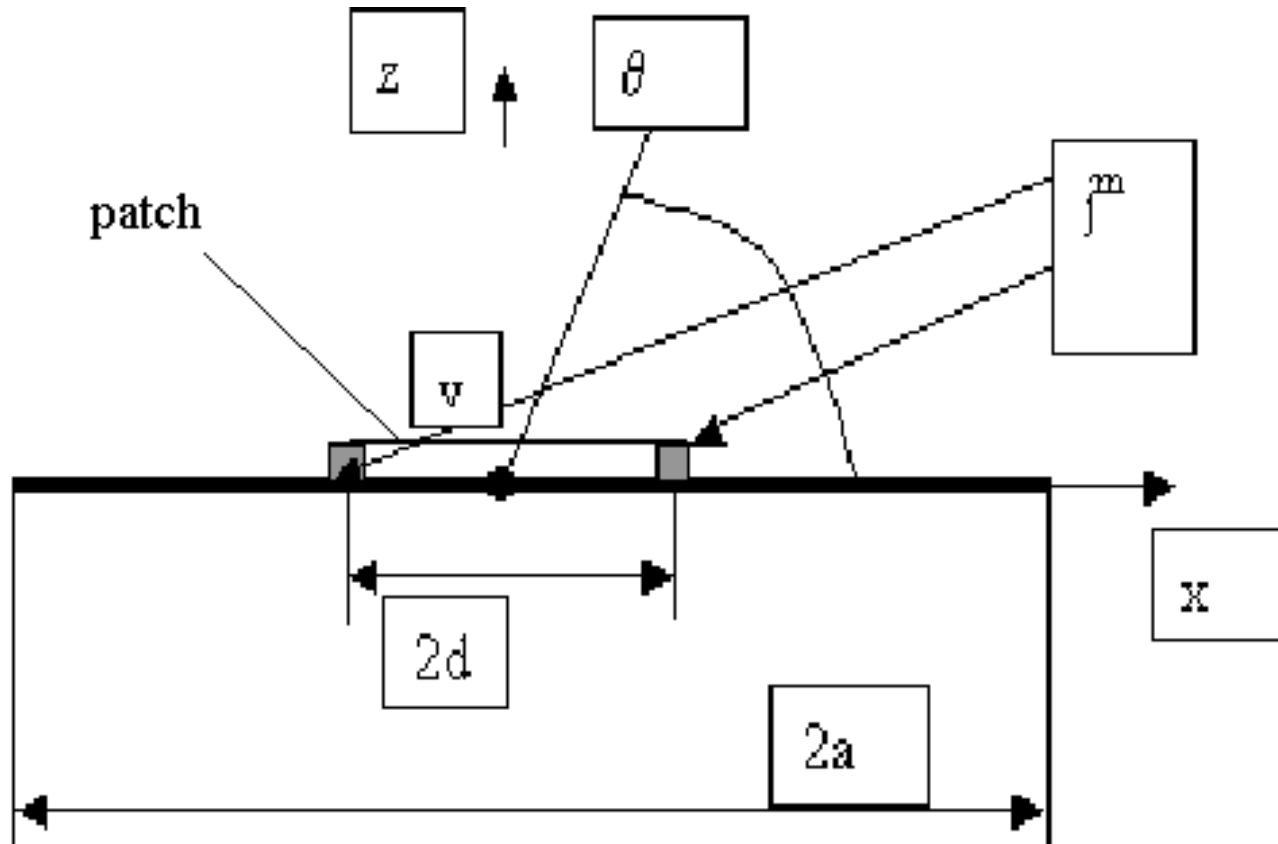
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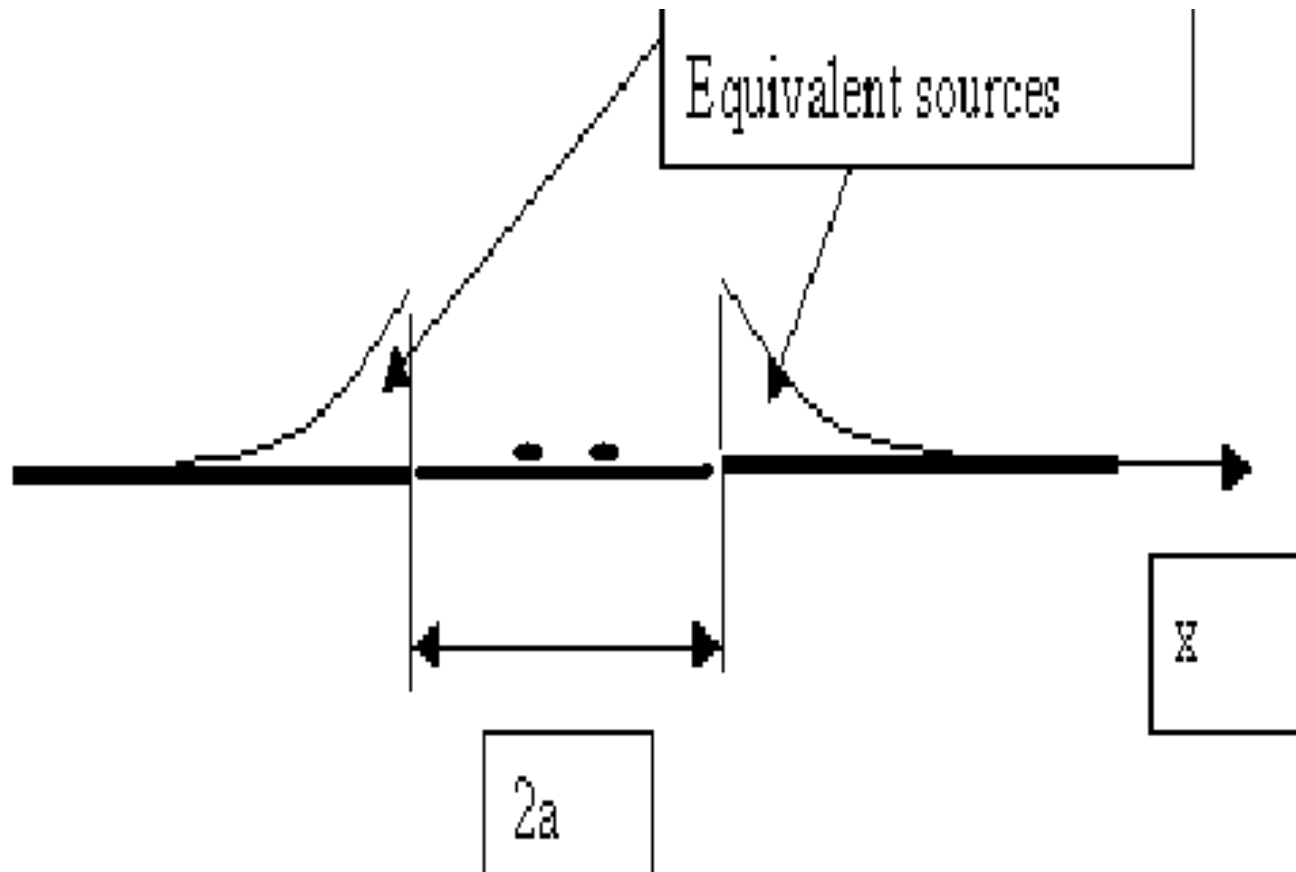
# 1. General considerations



- Transmitting mode; Natural scale:
- 2D problems; 1 wavelength = 20cm



# 1. Coventional Ground Planes



# 1.a) Flat Metal GroundPlane

## details of treatment

$$\vec{j}^m = U^m \delta(z) \delta(x-d) \vec{y}_0$$

$$\vec{H} = -\frac{k}{W_0} \frac{U^m}{4} H_0^{(2)}(kr) \vec{y}_0$$

$$\vec{j}^e = 2[\vec{z}_0, \vec{H}] = \frac{k}{W_0} \frac{U^m}{2} H_0^{(2)}(k|x-d|) \vec{x}_0 \approx \frac{k}{W_0} \frac{U^m}{2} \sqrt{\frac{2}{\pi k|x-d|}} e^{-i(k|x-d|-\frac{\pi}{4})} \vec{x}_0$$

$$E_{\theta 1} = \frac{k}{8} k U^m \sqrt{\frac{2}{\pi k r}} e^{-i(kr-\frac{\pi}{4})} \sin(\theta) \left\{ \int_a^\infty \sqrt{\frac{2}{\pi k(x-d)}} e^{-i(k(x-d)-\frac{\pi}{4})} e^{ikx \cos(\theta)} dx + \right.$$

$$\left. \int_{-\infty}^{-a} \sqrt{\frac{2}{\pi k(|x|+d)}} e^{-i(k(|x|+d)-\frac{\pi}{4})} e^{ikx \cos(\theta)} dx \right\}$$

$$\int_a^\infty \sqrt{\frac{2}{\pi k(x-d)}} e^{-i(k(x-d)-\frac{\pi}{4})} e^{ikx \cos(\theta)} dx \approx \frac{-i}{k} Al(a-d) \frac{e^{ika \cos(\theta)}}{1 - \cos(\theta)}$$

$$Al(s) = \sqrt{\frac{2}{\pi k s}} e^{-i(ks-\frac{\pi}{4})}$$

$$E_{\theta \text{diff}} = \frac{1}{8} k U^m \sqrt{\frac{2}{\pi k r}} e^{-i(kr-\frac{\pi}{4})} 2 \cos(kd) Al(a) \sin(\theta) \left\{ \frac{e^{ika \cos(\theta)}}{1 - \cos(\theta)} + \frac{e^{-ika \cos(\theta)}}{1 + \cos(\theta)} \right\}$$

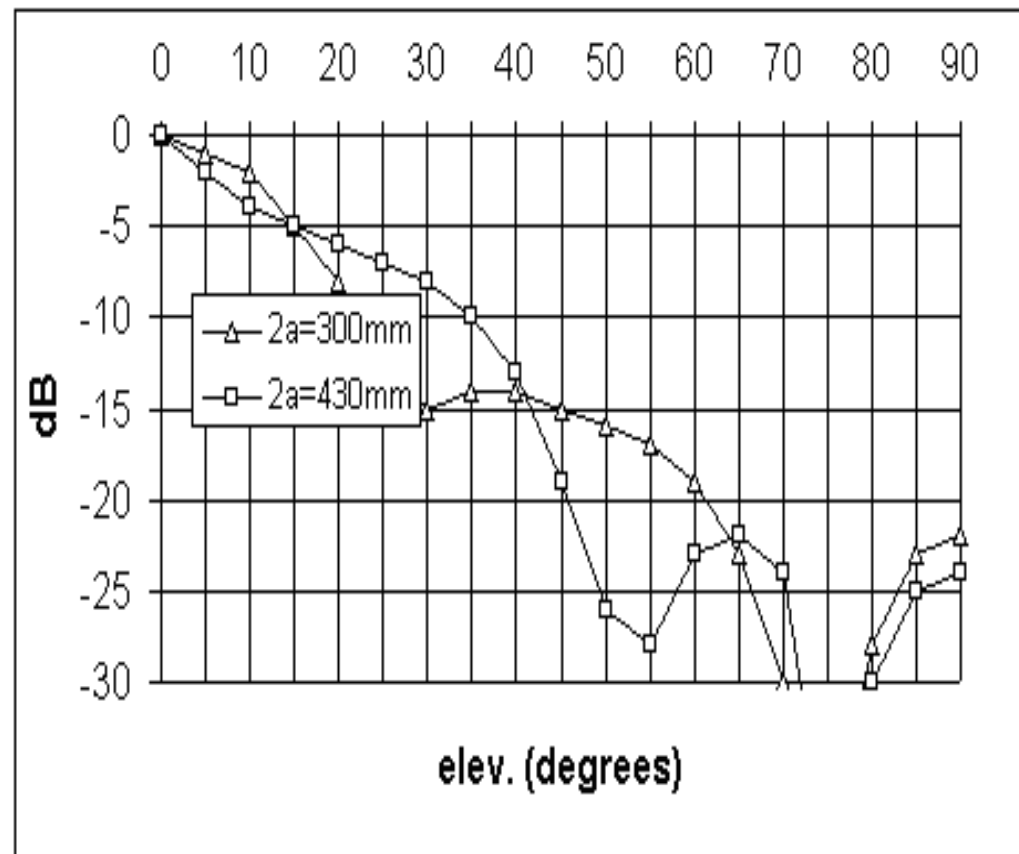
$$E_{\theta \text{inf}} = -\frac{1}{2} k U^m \sqrt{\frac{2}{\pi k r}} e^{-i(kr-\frac{\pi}{4})} 2 \cos(kd \cos(\theta))$$

$$\alpha \approx f_0(0) \frac{1}{2\pi \sqrt{\frac{a}{\lambda}}}$$

# 1.a) Flat Metal Ground Plane

$$j^e \approx \sqrt{\frac{1}{\frac{x}{\lambda}}}$$

$$\alpha \approx f_0(0) \frac{1}{2\pi \sqrt{\frac{a}{\lambda}}}$$



# 1.b) Impedance Ground Plane (e.g. Choke Ring) details of treatment

$$\vec{j}^m = \vec{y}_0 \frac{U^m}{2\pi} \delta(z-l) \int_{-\infty}^{\infty} e^{-iu(x-d)} du$$

$$E_x^- = \frac{1}{2} \frac{U^m}{2\pi} \int_{-\infty}^{\infty} e^{-i(u(x-d)-\zeta(z-l))} du$$

$$H_y^- = -\omega\epsilon_0 \frac{1}{2} \frac{U^m}{2\pi} \int_{-\infty}^{\infty} \frac{e^{-i(u(x-d)-\zeta(z-l))}}{\zeta} du$$

$$E_x^+ = \int_{-\infty}^{\infty} E_0^+(u) e^{-i(u(x-d)-\zeta(z-l))} du$$

$$H_y^+ = \omega\epsilon_0 \int_{-\infty}^{\infty} E_0^+(u) \frac{e^{-i(u(x-d)-\zeta(z-l))}}{\zeta} du$$

$$\zeta = \sqrt{k^2 - u^2}; \text{Re } \zeta \geq 0$$

$$E_x^{\text{total}} = -ZH_y^{\text{total}}$$

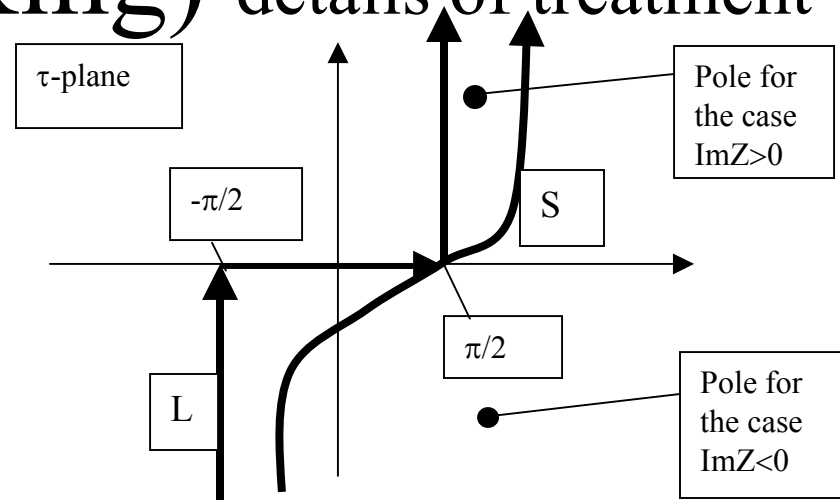
$$E_x^+(u) = -\frac{1}{2} \frac{U^m}{2\pi} \frac{1 - Z \frac{\omega\epsilon_0}{\zeta}}{1 + Z \frac{\omega\epsilon_0}{\zeta}} e^{-i\zeta l}$$

$$E_x^{\text{total}}(x)_{z=0} = \frac{U^m}{2\pi} Z \omega\epsilon_0 \int_{-\infty}^{\infty} \frac{1}{\zeta + Z \omega\epsilon_0} e^{-iu(x-d)} du$$

$$u = k \sin(\tau)$$

$$\text{Im}(Z) < 0$$

$$E_x^{\text{total}}(x) \approx -\frac{kU^m}{\sqrt{2\pi}} e^{i\frac{3\pi}{4}} \frac{W_0}{Z} \frac{e^{-ik|x-d|}}{(k|x-d|)^{3/2}}$$



$$H_y^{\text{total}} = -\frac{1}{Z} E_x^{\text{total}}(x) \approx \frac{kU^m}{W_0 \sqrt{2\pi}} e^{i\frac{3\pi}{4}} \left(\frac{W_0}{Z}\right)^2 \frac{e^{-ik|x-d|}}{(k|x-d|)^{3/2}}$$

$$E_{\theta 1} = -\frac{k}{4} \frac{kU^m}{\sqrt{2\pi}} e^{i\frac{3\pi}{4}} \frac{W_0}{Z} \sqrt{\frac{2}{\pi k r}} e^{-i(kr - \frac{\pi}{4})} \left(\frac{W_0}{Z} \sin(\theta) - 1\right)$$

$$\left\{ \int_a^{\infty} \frac{e^{-ik|x-d|}}{(k|x-d|)^{3/2}} e^{ikx \cos(\theta)} dx + \int_{-\infty}^{-a} \frac{e^{-ik|x-d|}}{(k|x-d|)^{3/2}} e^{ikx \cos(\theta)} dx \right\}$$

$$\int_a^{\infty} \frac{1}{(k(x-d))^{\frac{3}{2}}} e^{-ik(x-d)} e^{ikx \cos(\theta)} dx \approx \frac{-i}{k} A2(a-d) \frac{e^{ika \cos(\theta)}}{1 - \cos(\theta)}$$

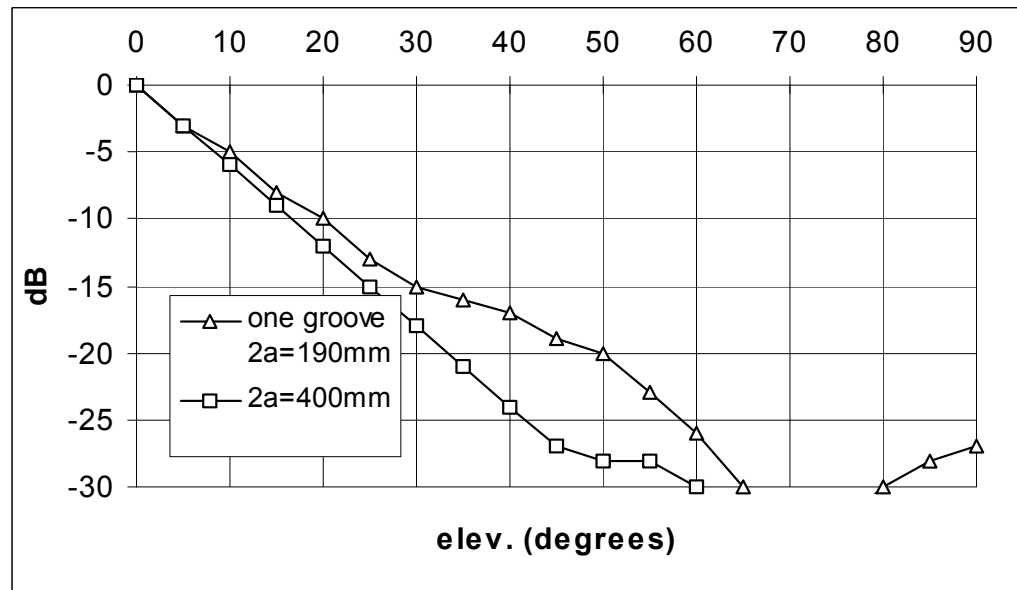
$$A2(s) = \frac{1}{(ks)^{\frac{3}{2}}} e^{-iks}; \alpha \approx f_0(0) \frac{\frac{W_0}{Z} (\frac{W_0}{Z} - 1)}{(2\pi)^2 \left(\frac{a}{\lambda}\right)^{3/2}}$$



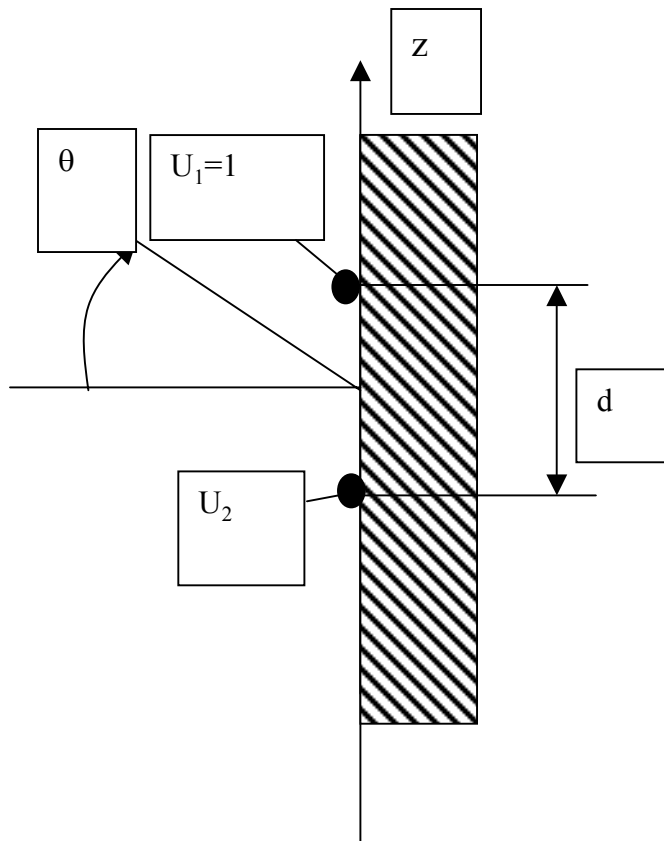
# 1.b) Impedance Ground Plane (e.g. Choke Ring)

$$|j^{equix}| = \left| \frac{j^{equim}}{Z} \right| \approx \frac{1}{(x/\lambda)^{3/2}}$$

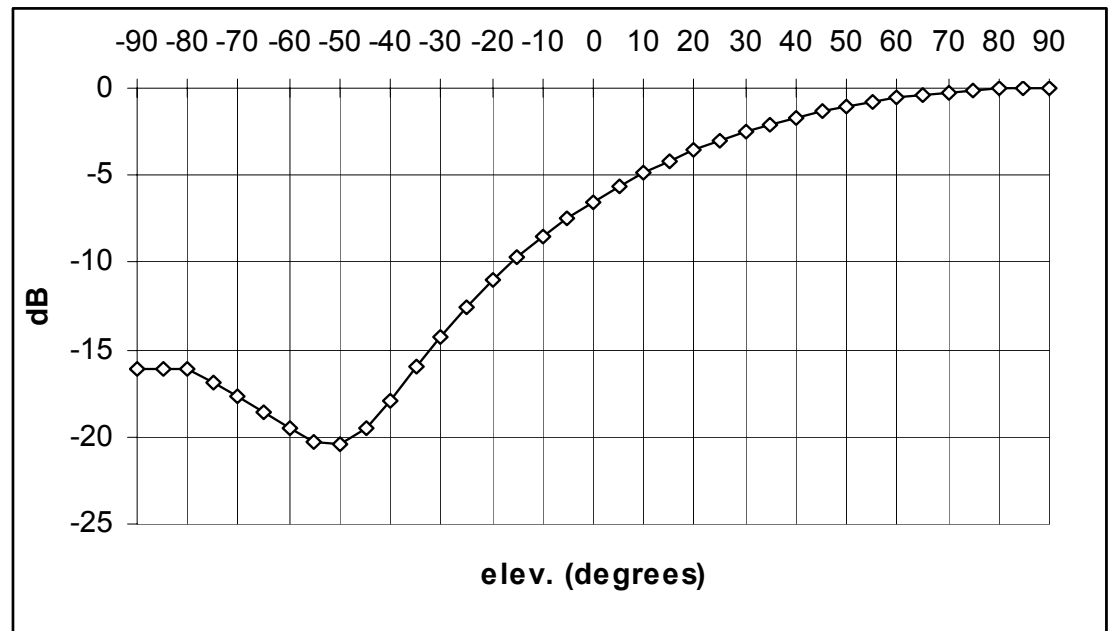
$$\alpha \approx f_0(0) \frac{\frac{W_0}{Z} (\frac{W_0}{Z} - 1)}{(2\pi)^2 \left(\frac{a}{\lambda}\right)^{3/2}}$$



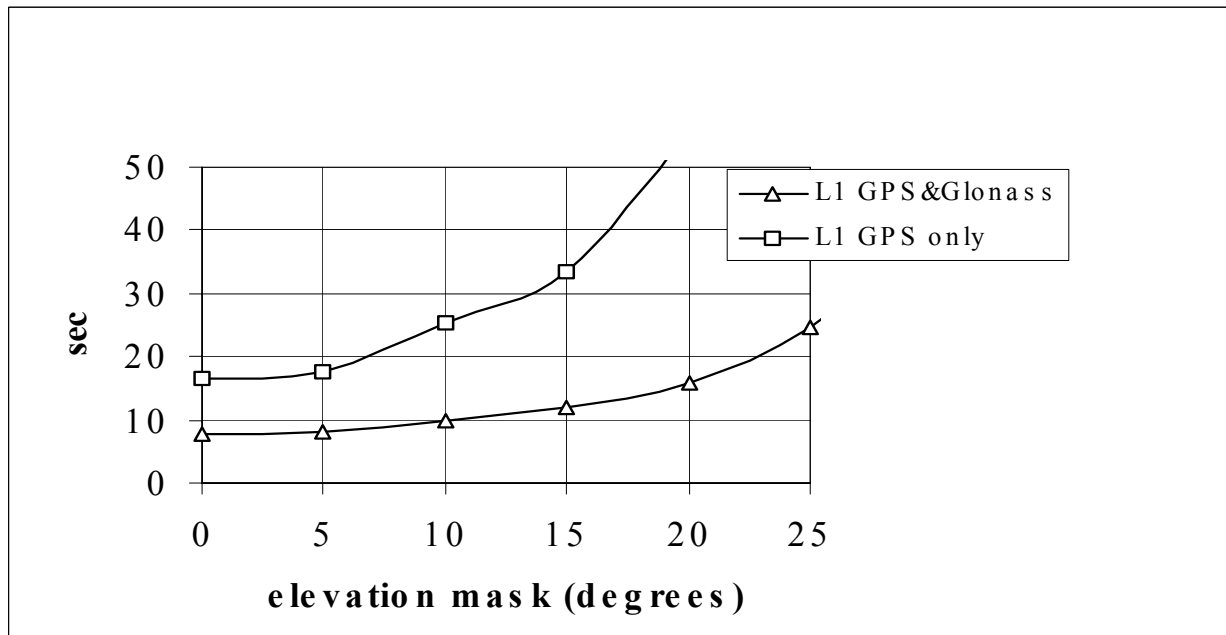
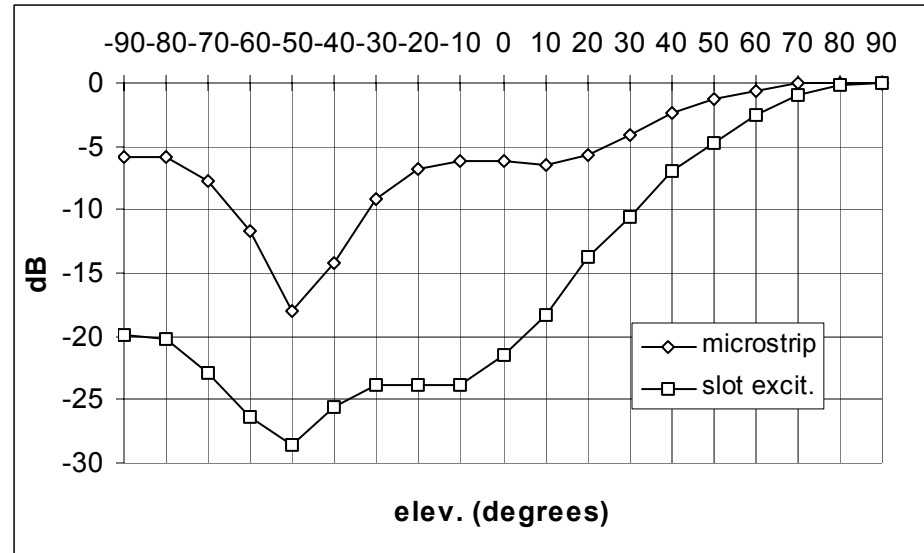
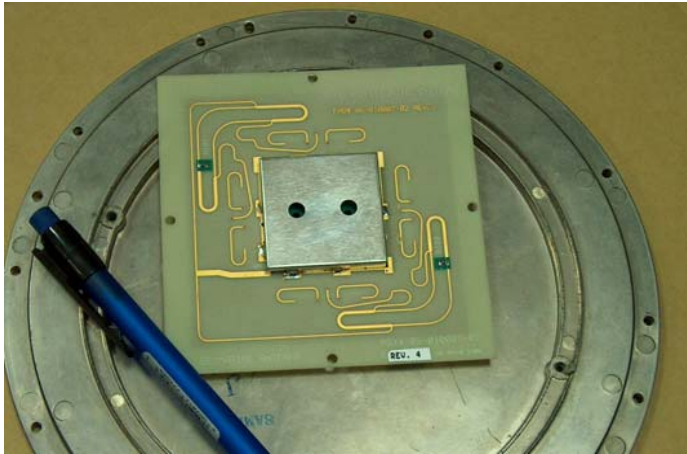
# 3. Small-size vertical structures

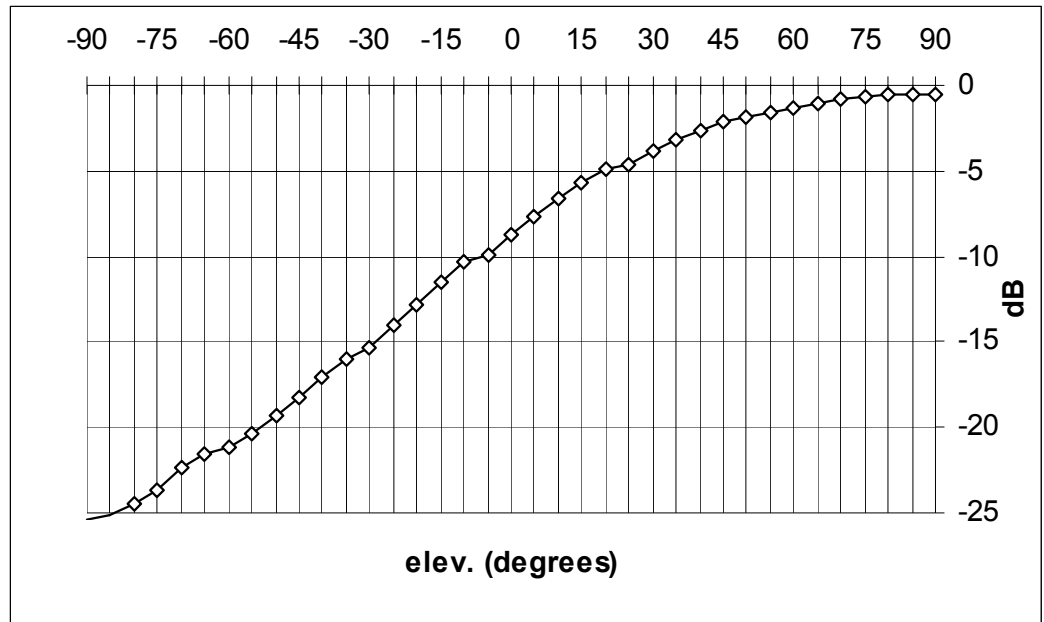


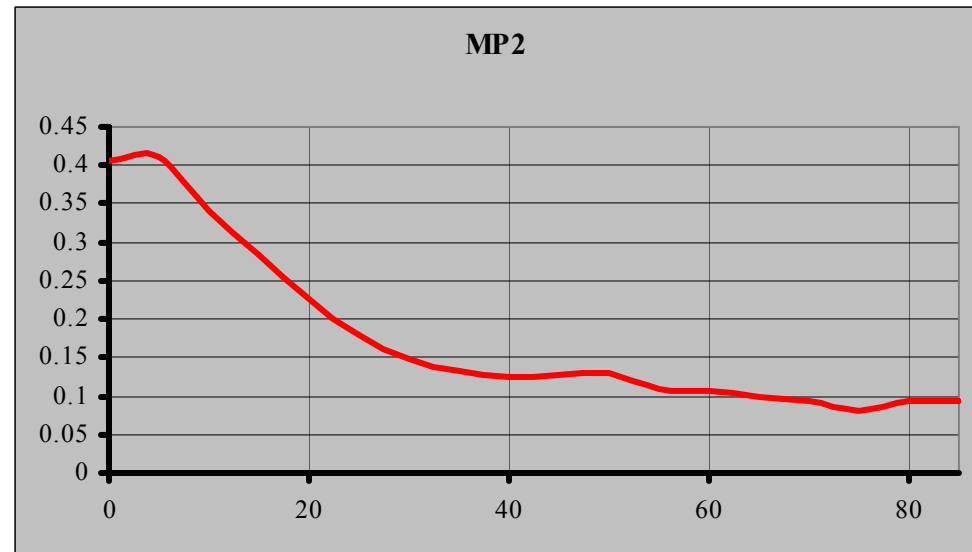
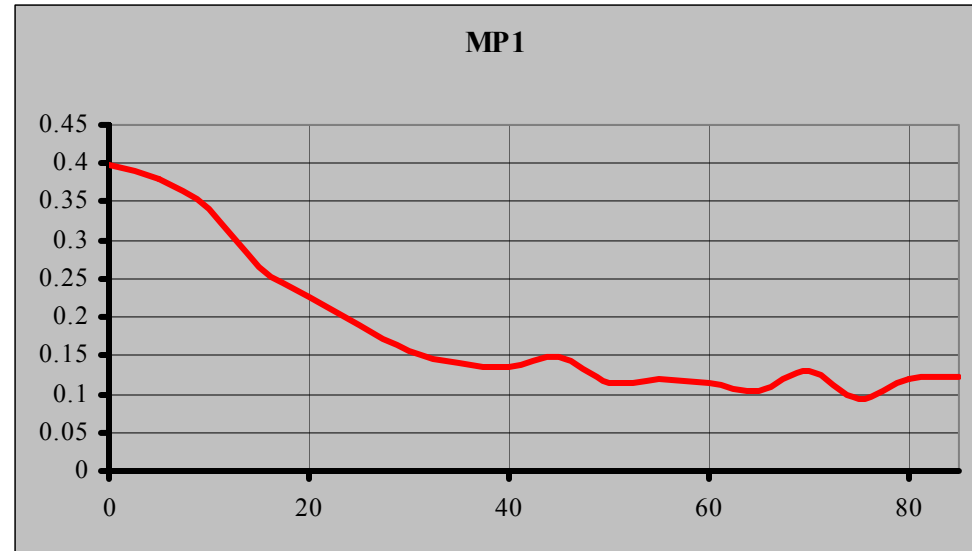
$d \ll \text{wavelength}(20\text{cm})$



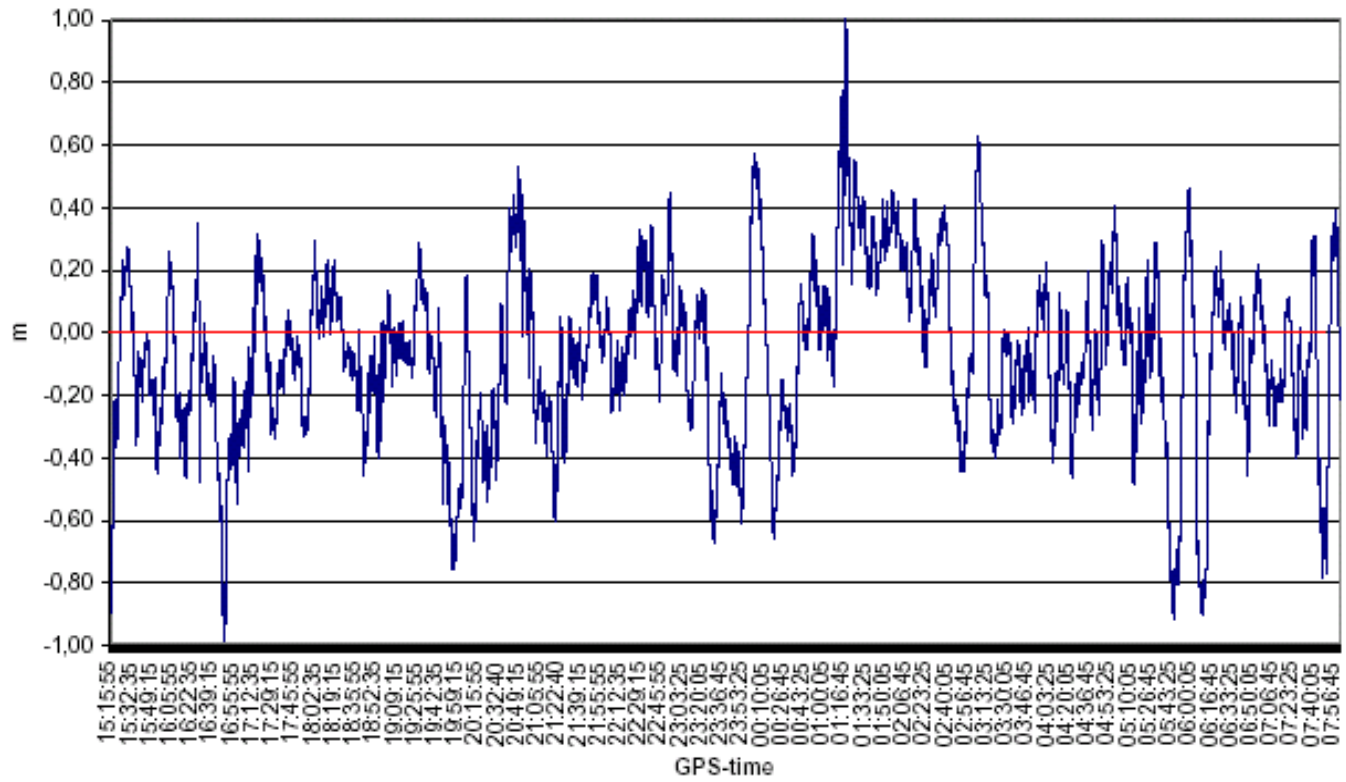
# 3. Practical results







Height: Divergence to known value  
Hannover - 09.12.03-10.12.03



# Conclusion

- Very small size multipath protected antennas might become a reality at least for RT positioning with about 1 cm accuracy though “superdirectivity” phenomena as theoretical limit should be considered .